## PATENT ABSTRACTS OF JAPAN

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(21)Application number: 10-085193 (71)Applicant: KYOCERA CORP

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31.03.1998 (72)Inventor: KIMURA TATSUYA

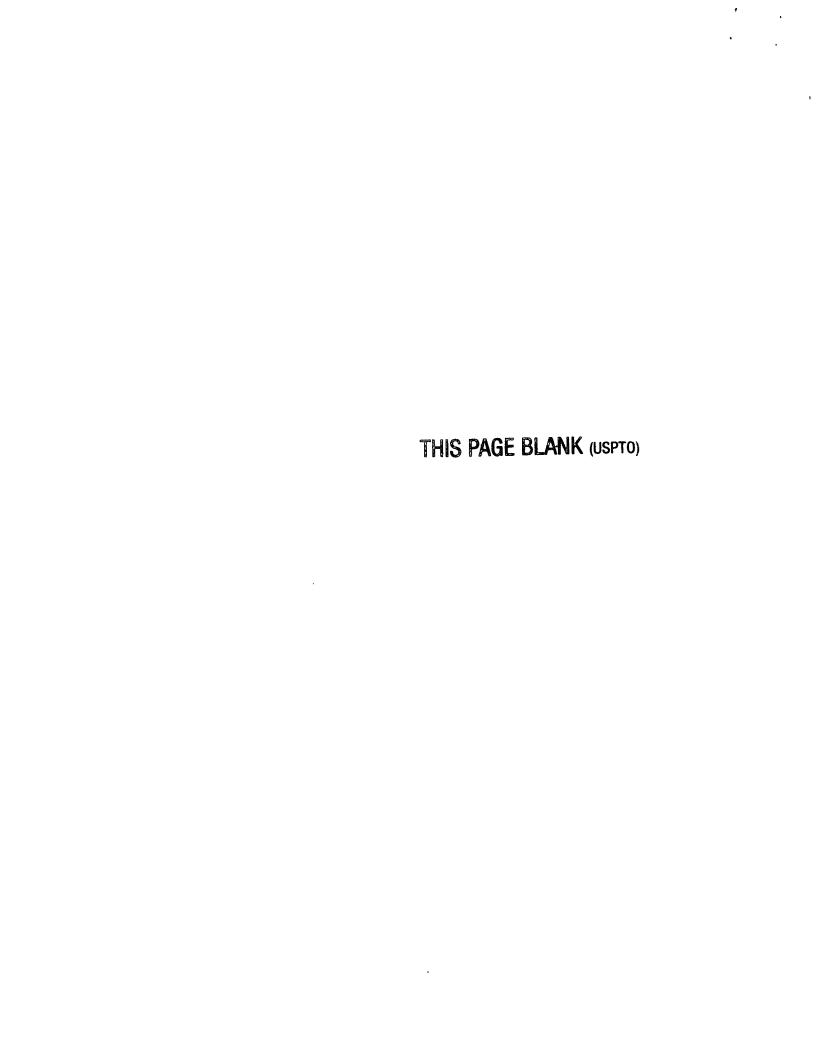
OTSUBO TAKASHIRO

# (54) SUBSTRATE FOR THIN FILM MAGNETIC HEAD AND THIN FILM MAGNETIC HEAD USING THAT

## (57)Abstract:

PROBLEM TO BE SOLVED: To improve heat radiating property by forming a first amorphous alumina film by sputtering and a second amorphous alumina film by ECR sputtering in this order to each specified film thickness on a substrate and then forming a magnetic film thereon.

SOLUTION: The substrate 6 consists of a dense sintered body of an Al2O3- TiC ceramic material, on which a first amorphous alumina film 7 and a second amorphous alumina film 8 are formed in lamination to give insulating property. The first amorphous alumina film 7 is formed to 0.2 to 2.0 µm thickness by sputtering. The second amorphous alumina film 8 is formed to 10 to 5500 & angst; by ECR sputtering. By forming two layers of the same compsn., good



adhesion property between the layers is obtd., and the probability to produce defects in the same position due to deposition of dust by sputtering is almost zero. Thus, the layers have high voltage resistance because no through defect is produced.

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## CLAIMS

[Claim(s)]

[Claim 1] The substrate for the thin film magnetic heads which comes to carry out the laminating of the 1st [ with a thickness of 0.2-2.4 micrometers formed by the sputtering method on the substrate ] amorphous alumina film, and the 2nd amorphous alumina film with a thickness [ by the ECR sputtering method ] of 10-5500A one by one.

[Claim 2] The thin film magnetic head which comes to form a magnetic film on the 2nd [ of the substrate for the thin film magnetic heads of claim 1 ] amorphous alumina film.

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## DETAILED DESCRIPTION

[Detailed Description of the Invention] [0001]

[Field of the Invention] This invention relates to the substrate for the thin film magnetic heads used for the thin film magnetic head and it which are used for the hard disk drive which is the recording apparatus of a computer, a tape drive, etc.

[0002]

[Description of the Prior Art] Conventionally, on the ceramic substrate which turns into a substrate for the thin film magnetic heads from an alumina (aluminum 2O3) and the composite of a titanium carbide (TiC) as a principal component, the insulator layer which consists of an amorphous alumina is formed by the sputtering method, and what carried out mirror plane processing of the field with the one side polish machine is used.

[0003] The above-mentioned insulator layer is formed in order to acquire insulation with the ceramic substrate which is electric conduction material, and to attain smooth nature further. Especially about the field coarseness of an insulator layer, in order to acquire a field important in order to form a component on it and smoother, it is processed by CMP (CHEMICAL MECHANICAL POLISHING) etc. [0004]

[Problem(s) to be Solved by the Invention] In order to raise recording density in recent years, it is shown that MR (MAGNETRORESISTIVE) which used the magneto-resistive effect for the component of the thin film magnetic head, or GMR (Giant MR) uses, but in the case of such MR component and a GMR component, in order to raise reading sensibility, it is necessary to raise a sense current value.

[0005] Moreover, in the MR head for hard disk drives, or a GMR head, with about 1 microinch, the flying height of a head is small and is becoming close to a NIAKON baton. Therefore, the so-called thermal asperity phenomenon which the magnetic head and media tend to carry out [ the phenomenon ] contact sliding, and a temperature change produces in MR component section of the thin film



magnetic head with the frictional heat at this time, consequently reading sensibility reduces serves as a very big trouble.

[0006] In order to cancel this trouble, it is necessary to raise the heat dissipation nature of the circumference of a component, therefore the substrate film of MR component is formed by high temperature conduction material, such as AlN, and the technique of raising the heat dissipation nature of the circumference of a component is proposed.

[0007] However, if film formation is carried out with the above-mentioned high temperature conduction insulating material, membrane stress will become very high, therefore if thickness is set to 2 micrometers or more, a substrate will deform, and exfoliation arises. On the other hand, if it is made less than 2-micrometer thickness, electric pressure=proofing will become inadequate, and sufficient thickness to carry out polish processing of the membrane formation side moreover is not obtained.

[0008] Then, thickness of said amorphous alumina film is made thin, MR component is brought close to the high aluminum2 O3-TiC substrate of heat conduction, heat dissipation nature is raised by this, or the recess by the hardness difference of an aluminum2 O3-TiC substrate and the amorphous alumina film is used, and the cure of preventing that MR component collides with a media side is performed.

[0009] However, when the thickness of the amorphous alumina film was set to 3 micrometers or less, it was inadequate in respect of withstand voltage.

[0010] Therefore, the object of this invention is offering the substrate for the thin film magnetic heads which prevented the contact to the media side of a component and was further excellent in film adhesion reinforcement, electric pressure-proofing, and field grace while it makes thickness of the amorphous alumina film thin and raises the heat dissipation nature of the thin film magnetic-head component section by this.

[0011] Other objects of this invention are to offer the thin film magnetic head of the high quality which used the substrate for the thin film magnetic heads of this

invention, and high-reliability.

[0012]

[Means for Solving the Problem] The substrate for the thin film magnetic heads of this invention is characterized by carrying out the laminating of the 1st [ with a thickness of 0.2-2.4 micrometers formed by the sputtering method on the substrate ] amorphous alumina film, and the 2nd amorphous alumina film with a thickness [ by the ECR sputtering method ] of 10-5500A one by one. [0013] It is characterized by the thin film magnetic head of this invention coming to form a magnetic film on the 2nd [ of the substrate for the thin film magnetic heads of this invention ] amorphous alumina film.

[0014]

[Embodiment of the Invention] Hereafter, drawing 1 - drawing 4 explain the operation gestalt of this invention. The perspective view in which (a) of drawing 1 and (b) show the substrate 1 for the thin film magnetic heads of this invention, the important section expanded sectional view by cutting plane line X-X [ in / in drawing 2 / drawing 1 R> 1 (a) ], and drawing 3 are the important section expanded sectional views showing the layer system in which the magnetic film was formed on the substrate 1 for the thin film magnetic heads of this invention. Moreover, drawing 4 is the sectional view showing the busy condition of the thin film magnetic head 2 of this invention.

[0015] As for the slider with which 3 consists of the aluminum2 O3-TiC system ceramics, a ferrite, sapphire, etc., and 4, in the thin film magnetic head 2 of drawing 4, MR component and 5 are media.

[0016] The above-mentioned thin film magnetic head 2 is obtained according to the following production process. First, according to the substrate 1 for the thin film magnetic heads of drawing 1, as shown in the disc-like substrate 6 with a diameter of 2-8 inches which has an orientation flat as shown in (a), or (b), it is the 3-6 inches one-side corner guard-like substrate 6. On these substrates 6, as shown in drawing 2, the 1st amorphous alumina film 7 is formed by the sputtering method, and subsequently the 2nd amorphous alumina film 8 is

formed.

[0017] The 2nd amorphous alumina film 8 is having formed by the ECR sputtering method, the surface 8a becomes a very smooth field, and as shown in drawing 3, it forms a magnetic film 9 on surface 8a. pass a slicing process, an ABS side polish process, and ion milling processing (RIE processing) one by one after such a wafer process -- much thin film magnetic heads 2 are obtained simultaneously. About MR component, it is the component used by reading and forms with the ultra-fine processing technology by photograph RISOGURAFU. [0018] the case where the above-mentioned substrate 6 is produced with the aluminum2 O3-TiC system ceramics -- 60 - 80% of aluminum 2O3 the raw material which uses 40 - 20% of TiC as a principal component -- using -- the inside of atmospheric air or reducing atmosphere -- 1600-1800 degrees C -- a hotpress -- or HIP processing is carried out and it is obtained. This aluminum2 O3-TiC system ceramics serves as a very precise sintered compact, and can smooth a front face.

[0019] Although such aluminum2 O3-TiC system ceramics is electric conduction material, it gives insulation by forming the 1st and 2nd amorphous alumina film 7 and 8 on a substrate 6.

[0020] Although formed by the sputtering method about the 1st amorphous alumina film 7, dust adhesion in the substrate at the time of a spatter mainly originates, and it is easy to generate many defects in the film. Then, it is good to fly the dust by performing Ar ion etching processing within a sputtering system. [0021] Moreover, it faces forming the 2nd amorphous alumina film 8, and there is almost that no dust adheres to the same part as adhesion of the dust in membrane formation formation of the 1st amorphous alumina film 7 in the film 8, therefore defective generating about the said division can be prevented, and the 2nd amorphous alumina film 8 which has the high withstand voltage which does not have the penetrated defect by this is obtained.

[0022] And high adhesion is acquired between two-layer by carrying out membrane formation formation of the both sides with the same amorphous



alumina film in this way.

[0023] Moreover, if the 2nd amorphous alumina film 8 is formed by the ECR sputtering method, if the front face is expressed with the surface roughness (Ra) measured by AFM (ATOMIC FORCE MICROSCOPY), it will be made to 10A or less. And after forming the 2nd amorphous alumina film 8 by the ECR sputtering method, CMP processing may be carried out that a film front face should be made still smoother.

[0024] Although many defects have occurred in the film by the 1st amorphous alumina film 7 formed by the sputtering method as mentioned above, by the 2nd amorphous alumina film 8 further formed by the ECR sputtering method, a high membrane formation filling factor is obtained, a high film degree of hardness can be attained, and there is the operation effectiveness as following by this.

[0025] (1) By forming the thermally conductive low film thinly, a twist can burn heat, it can tell at the thermally conductive high slider 3, and heat dissipation nature is raised by this.

[0026] (2) Since it becomes the thin substrate film of thickness, contact can be prevented by the recess (level difference shown in drawing 4) which a component approaches a slider 3, therefore is generated at the time of the lap of an ABS side.

[0027] (3) Since the 1st amorphous alumina film 7 and the 2nd amorphous alumina film 8 have the same construction material, the film adhesion reinforcement between both sides becomes high.

[0028] (4) Electric pressure-proofing is raised by having formed the 2nd amorphous alumina film 8 by the ECR sputtering method (the ordinary temperature resistance in applied-voltage 10V to the laminating of the 1st and 2nd amorphous alumina film 7 and 8 is set to 1011ohms or more).

[0029] (5) Improve that the 2nd amorphous alumina film 7 is also about the 1st amorphous alumina film 8 inferior to field granularity, and offer the substrate 1 for the thin film magnetic heads excellent in field grace.

[0030] Moreover, it is good to make thickness of the 1st amorphous alumina film

7 to 0.2-2.0 micrometers, and to make suitably 0.2-2.4 micrometers of 10-5500A of thickness of the 2nd amorphous alumina film 8 into 10-5000A. [0031] If polish processing becomes difficult, and an insulating property is not acquired but 2.4 micrometers is exceeded when the thickness of the 1st amorphous alumina film 7 is less than 0.2 micrometers, heat dissipation nature will deteriorate and the contact to the media of a component will arise. If an insulating property is not acquired but 5500A is exceeded when the thickness of the 2nd amorphous alumina film 8 is less than 10A, exfoliation will occur with membranous stress.

[0032] In this invention, after forming the 1st amorphous alumina film 7 by the sputtering method, it is good to grind the front face smoothly further again. Therefore, it is good to make into 5A or less field relative roughness which performs CMP processing and is measured by AFM by Ra. [0033]

[Example] Hereafter, the example of this invention is explained. The alumina (the mean diameter of 99.9% of purity and raw-material powder: 0.4 micrometers) and the titanium carbide (the mean diameter of 99.5% of purity and raw-material powder: 0.3 micrometers) were used as a start raw material, weighing capacity was carried out so that an alumina might serve as and a titanium carbide might serve as 30% of the weight of a ratio 70% of the weight, about 10% of the weight of titanium oxide TiO2 was further added to the titanium carbide, and it mixed with alumina balls. Subsequently, mixed powder is fabricated and they are 1600 degrees C and 250kg/cm2. Hotpress baking was carried out by the pressure for 1 hour.

[0034] Thus, after carrying out the grinding process of the produced sintered compact to the shape of a predetermined disk type by the diamond wheel, surface wrapping processing was performed using the diamond abrasive grain. Subsequently, using diamond powder with a mean particle diameter of 0.5 micrometers, a substrate front face, a polish plate, or abrasive cloth was slid relatively, precision polish was performed, and surface roughness Ra of a

substrate was made into 18A by this. In this example, the tin surface plate was used as the above-mentioned polish plate.

[0035] The alumina target of 99.5% of purity is used as shown in a table 1. And by the sputtering method After it forms an amorphous alumina and the polish liquid which made spherical alumina impalpable powder suspend in pure water performs mirror plane processing after that, The polish liquid which made spherical Seria impalpable powder suspend in pure water performed the last precision processing, and 1-4 micrometers of thickness and the 1st film surface (surface roughness Ra) 3A amorphous alumina film were formed the passage of sample No.1-12.

[0036] About sample No.7-12, the 2nd amorphous alumina film which changed thickness also into \*\* and a cage was formed using the ECR sputtering method as shown in this table after an appropriate time. Furthermore it replaces with the 2nd amorphous alumina film, and the case where continued the amorphous alumina film by the usual sputtering method, and membranes are formed is shown as sample No.5 and sample No.6.

[0037] Moreover, about sample No.6, and 8 and 10, precision mirror plane processing was performed with the polish liquid which made spherical Seria impalpable powder suspend in pure water.

[0038]

[A table 1]

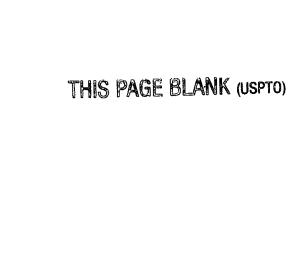
試料 No		第1の 『モルファスアルミナ膜 厚み(μm)	第2の圧われながけ膜		加熱処理	表面租度	抵抗值
			製法 (μm)	鏡面	後膜剝離	Ra (Å)	Ω
*	1	4			無	3	1011
*	2	3		_	無	3	10 4
*	3	2		_	無	3	10 4
*	4	1		_	無	3	10'
*	5	2	スパッタ (1 μm)	無	無 無	1 2	1010
*	6	2	スメ゙ッタ (0.3 μ m)	有	無	3	10 9
	7	2	ECR (5000 Å)	無	無	5	1013
	8	2	ECR (1500 Å)	有	無	3	1 0 12
	9	2	ECR (100 Å)	無	無	4	1011
1	0	1	ECR (1500 Å)	有	無	3	1 0 12
1	1	1	ECR (50 Å)	無	無	4	1011
<b>※</b> 1	2	1	ECR (6000 Å)	無	有	6	1 0 12

※印の試料Noは本発明の範囲外のものである。

[0039] When the film exfoliation, the surface roughness, and the resistance after heat-treatment were measured to each [ these ] sample, the result as shown in this table was obtained.

[0040] About the film exfoliation after heat-treatment, each sample was heated at the temperature of 600 degrees C within the vacuum ambient atmosphere, and the desquamative state of a membrane formation phase was checked with the differential interference microscope (50 times). Moreover, the surface roughness on the front face of the outermost was measured in AFM.

[0041] About ordinary temperature resistance, 20 place / phi 4 microinches of electrodes of Ti/Au were formed in the film surface, it had in ordinary temperature applied-voltage 10V, the resistance between a film front face and the rear face of



a substrate was measured using the 3 terminal method, and the minimum resistance was calculated.

[0042] Even if it set thickness of the amorphous alumina film to less than 2.5 micrometers about sample No.7-11 of this invention the passage clear from the result shown in a table 1, resistance was set to 1011ohms or more, the outstanding withstand voltage was obtained, film exfoliation stops having arisen after heat-treatment further, and surface roughness Ra became 5A or less. [0043] When the amorphous alumina film was attached by the ECR spatter, there was an inclination for field granularity to become large, but on the other hand the very high-density film could be formed and the very smooth field which does not exceed Ra10A with the field relative roughness of a membrane formation side, either was acquired. In addition, if it is such high density film, a still smoother field will be acquired by carrying out CMP processing.

[0044] However, when it is only the 1st amorphous alumina film a passage clear from sample No.1-4, unless it forms thickness 4 micrometers or more, the resistance of 1011ohms or more is not acquired.

[0045] moreover, sample No. -- if it is the case where the 2nd amorphous alumina film is formed by the sputtering method a passage clear from 5 and 6 even if it made it the two-layer film, as shown in sample No.2 and sample No.5, the same thickness will also serve as resistance of less than 1011ohms by 3 micrometers or less of thickness, although resistance tends to become high. [0046] Since the stress by the consistency difference between two-layer film was too high further again when the 2nd amorphous alumina film is formed by the thickness of 6000A the passage of sample No.12, film exfoliation arose in the heat-treatment in a vacuum.

[0047]

[Effect of the Invention] It is having carried out the laminating of the 2nd amorphous alumina film with a thickness of 10-5500A formed in this invention by the 1st amorphous alumina film and ECR sputtering method with a thickness of 0.2-2.4 micrometers which were formed by the sputtering method on the

substrate as above one by one. While raising the heat dissipation nature of the thin film magnetic-head component section, the contact to the media side of a component was prevented and the substrate for the thin film magnetic heads which was further excellent in film adhesion reinforcement, electric pressure-proofing, and field grace has been offered.

[0048] Moreover, in this invention, it is having used the substrate for the thin film magnetic heads of this invention, and the thin film magnetic head of high quality and high-reliability has been offered.

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## DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[Drawing 1] (a) And (b) is the perspective view showing the substrate for the thin film magnetic heads of this invention.

[Drawing 2] It is an important section expanded sectional view by cutting plane line X-X in drawing 1 (a).

[Drawing 3] It is the important section expanded sectional view showing the layer system of the thin film magnetic head of this invention.

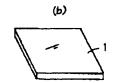
[Drawing 4] It is the explanatory view showing the busy condition of the thin film

magnetic head of this invention.
[Description of Notations]
1 Substrate for Thin Film Magnetic Heads
2 Thin Film Magnetic Head
3 Slider
4 MR Component
5 Media
6 Substrate
7 1st Amorphous Alumina Film
8 2nd Amorphous Alumina Film
9 Magnetic Film
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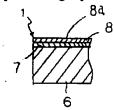
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# [Drawing 1]

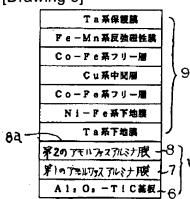




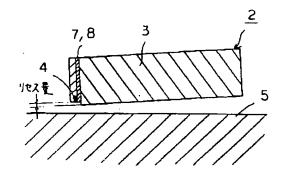
## [Drawing 2]



# [Drawing 3]



[Drawing 4]



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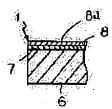
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(71)出願人 000006633

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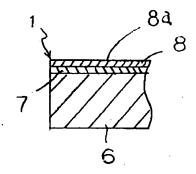
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## (57)【要約】

【課題】薄膜磁気ヘッド素子部の放熱性を上げるとともに、素子のメディア面への接触を防止し、さらに膜密着強度、電気的な耐圧、面品位に優れた薄膜磁気ヘッド用基板を提供する。

【解決手段】基板6上にスパッタリング法により形成した厚み0.2~2.4μmの第1のアモルファスアルミナ膜7と、ECRスパッタリング法により形成した厚み10~5500Åの第2のアモルファスアルミナ膜8とを順次積層してなる薄膜磁気ヘッド用基板1。



1

## 【特許請求の範囲】

【請求項1】基板上にスパッタリング法により形成した厚み0.2~2.4 $\mu$ mの第1のアモルファスアルミナ膜と、ECRスパッタリング法による厚み10~5500Aの第2のアモルファスアルミナ膜とを順次積層してなる薄膜磁気ヘッド用基板。

【請求項2】請求項1の薄膜磁気ヘッド用基板の第2のアモルファスアルミナ膜上に磁性膜を形成してなる薄膜磁気ヘッド。

## 【発明の詳細な説明】

#### [0001]

【発明の属する技術分野】本発明はコンピューターの記録装置であるハードディスクドライブやテープドライブ等に用いられる薄膜磁気ヘッドならびにそれに用いる薄膜磁気ヘッド用基板に関するものである。

## [0002]

【従来の技術】従来、薄膜磁気ヘッド用基板には主成分としてアルミナ(Al2 O3) およびチタンカーバイド (TiC) の複合材からなるセラミック基板上にアモルファスアルミナからなる絶縁膜をスパッタリング法にて成膜し、その面を片面ポリッシュ機にて鏡面加工したものが用いられている。

【0003】上記絶縁膜は導電材であるセラミック基板との絶縁性を得るため、さらに平滑性を達成するために形成している。とくに絶縁膜の面粗さについては、その上に素子を形成するために重要であって、より平滑な面を得るためにCMP(CHEMICAL MECHANICAL POLISHING)等で加工している。

## [0004]

【発明が解決しようとする問題点】近年、記録密度を向上させるために、薄膜磁気ヘッドの素子に磁気抵抗効果を用いたMR(MAGNETRORESISTIVE)、あるいはGMR(Giant MR)が用いることが提示されているが、このようなMR素子やGMR素子の場合、読み取り感度を向上させるためにセンス電流値を上げる必要がある。

【0005】また、ハードディスクドライブ用MRへッドやGMRへッドにおいては、ヘッドの浮上量が1マイクロインチ程度と小さく、ニアコンタクトに近くなってきている。そのため磁気ヘッドとメディアが接触摺動しやすく、この時の摩擦熱により薄膜磁気ヘッドのMR素子部に温度変化が生じ、その結果、読み取り感度が低減する、いわゆるサーマルアスペリティ現象が非常に大きな問題点となってきた。

【0006】かかる問題点を解消するために、素子周りの放熱性を上げる必要があり、そのためにMR素子の下地膜をA1Nなどの高熱伝導材で形成し、素子周りの放熱性を上げるという技術が提案されている。

【0007】しかしながら、上記高熱伝導絶縁材により 膜形成すると、膜応力が非常に高くなり、そのために膜 50 厚を  $2 \mu$  m以上にすると基板が変形し、剥離が生じる。 他方、  $2 \mu$  m未満の膜厚にすると電気的な耐圧が不十分 となり、しかも、成膜面をポリッシュ加工するに十分な 膜厚が得られない。

【0008】そこで、前記アモルファスアルミナ膜の厚みを薄くして、MR素子を熱伝導の高いA12 O3 -TiC基板に近づけ、これによって放熱性を上げたり、もしくはA12 O3 -TiC基板とアモルファスアルミナ膜との硬度差によるリセスを利用し、MR素子がメディア面と衝突することを防止する等の対策がおこなわれている。

【0009】しかしながら、アモルファスアルミナ膜の膜厚が $3\mu$ m以下になると、耐電圧の点で不十分であった。

【0010】したがって、本発明の目的はアモルファスアルミナ膜の厚みを薄くし、これによって薄膜磁気ヘッド素子部の放熱性を上げるとともに、素子のメディア面への接触を防止し、さらに膜密着強度、電気的な耐圧、面品位に優れた薄膜磁気ヘッド用基板を提供することである。

【0011】本発明の他の目的は本発明の薄膜磁気ヘッド用基板を用いた高品質かつ高信頼性の薄膜磁気ヘッドを提供することにある。

#### [0012]

【問題点を解決するための手段】本発明の薄膜磁気ヘッド用基板は、基板上にスパッタリング法により形成した厚み0.2~2.4  $\mu$  mの第1のアモルファスアルミナ膜と、ECRスパッタリング法による厚み10~5500Åの第2のアモルファスアルミナ膜とを順次積層したことを特徴とする。

【0013】本発明の薄膜磁気ヘッドは、本発明の薄膜磁気ヘッド用基板の第2のアモルファスアルミナ膜上に磁性膜を形成してなることを特徴とする。

## [0014]

【発明の実施の形態】以下、本発明の実施形態を図1〜図4によって説明する。図1の(a)および(b)は本発明の薄膜磁気ヘッド用基板1を示す斜視図、図2は図1(a)における切断面線X-Xによる要部拡大断面図、図3は本発明の薄膜磁気ヘッド用基板1の上に磁性膜を形成した層構造を示す要部拡大断面図である。また、図4は本発明の薄膜磁気ヘッド2の使用状態を示す断面図である。

【0015】図4の薄膜磁気ヘッド2において、3はA l2 O3 - Ti C系セラミックス、フェライト、サファ イアなどからなるスライダ、4はMR素子、5はメディ アである。

【0016】上記薄膜磁気ヘッド2は下記の製造工程により得られる。まず、図1の薄膜磁気ヘッド用基板1によれば、(a)に示すようにオリエンテーションフラットを有する直径2~8インチの円板状基板6、もしくは

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(b) に示すように一辺3~6インチの角板状基板6である。これらの基板6の上に、図2に示すように第1のアモルファスアルミナ膜7をスパッタリング法により形成し、ついで第2のアモルファスアルミナ膜8を形成する。

【0017】第2のアモルファスアルミナ膜8はECRスパッタリング法により形成したことで、その表面8aはきわめて滑らかな面となり、図3に示すように表面8aの上に磁性膜9を形成する。このようなウエハ工程の後に、スライシング工程、ABS面ポリッシュ工程、イオンミリング加工(RIE加工)を順次経て、多数の薄膜磁気ヘッド2を同時に得る。MR素子については、読み込みで使用する素子であって、フォトリソグラフによる微細加工技術で形成する。

【0018】上記基板6をA12 O3 - TiC系セラミックスで作製する場合には、60~80%のA12 O3 と40~20%のTiCを主成分とする原料を用い、大気あるいは還元雰囲気中1600~1800℃でホットプレスあるいはHIP処理して得られる。このA12 O3 - TiC系セラミックスは非常に緻密な焼結体となり、表面を滑らかにすることができる。

【0019】このようなAl2 O3 - TiC系セラミックスは導電材であるが、基板6上に第1、第2のアモルファスアルミナ膜7、8を形成することによって絶縁性をもたせる。

【0020】第1のアモルファスアルミナ膜7については、スパッタリング法により形成するが、スパッタ時の基板へのゴミ付着が主に起因して、膜内には多くの欠陥が発生しやすい。そこで、スパッタリング装置内でArイオンエッチング処理をおこなうことで、そのゴミを飛 30 ばすのがよい。

【0021】また、第2のアモルファスアルミナ膜8を 形成するに際して、その膜8には第1のアモルファスア ルミナ膜7の成膜形成でのゴミの付着と同一の部位にゴ ミが付着することはほとんどなく、そのために同部位で の欠陥発生が防止でき、これにより、質通した欠陥のな い高い耐電圧を有する第2のアモルファスアルミナ膜8 が得られる。

【0022】そして、このように双方を同じアモルファスアルミナ膜により成膜形成することで、2層間で高い 40 密着性が得られる。

【0023】また、ECRスパッタリング法により第2のアモルファスアルミナ膜8を形成すれば、その表面はAFM (ATOMIC FORCE MICROSCOPY)で測定される表面粗度(Ra)であらわすと、10A以下にできる。そして、第2のアモルファスアルミナ膜8をECRスパッタリング法により形成した後に、膜表面をさらに平滑にすべくCMP加工してもよい。

【0024】上記のようにスパッタリング法により形成 し、1600℃、25 した第1のアモルファスアルミナ膜7では、膜内に多く 50 ットプレス焼成した。

の欠陥が発生しているが、さらにECRスパッタリング 法により形成した第2のアモルファスアルミナ膜8では 高い成膜充填率が得られ、高い膜硬度が達成でき、これ によって下記のとおりの作用効果がある。

【0025】(1)熱伝導性の低い膜を薄く形成することで、熱伝導性の高いスライダ3に熱をよりはやく伝えることができ、これによって放熱性が高められる。

【0026】(2) 膜厚の薄い下地膜となるので、素子がスライダ3に近づき、そのためにABS面のラップ時に発生するリセス(図4に示す段差)により接触が防止できる。

【0027】(3) 第1のアモルファスアルミナ膜7と 第2のアモルファスアルミナ膜8とは材質が同じである ために、双方間の膜密着強度は高くなる。

【0028】 (4) 第2のアモルファスアルミナ膜8を ECRスパッタリング法により形成したことで、電気的 耐圧が高められる(第1、第2のアモルファスアルミナ 膜7、8の積層に対する印加電圧10 Vにおける常温抵 抗値は10 $^{11}$   $\Omega$ 以上となる)。

20 【0029】(5)面粗さに劣る第1のアモルファスアルミナ膜8を第2のアモルファスアルミナ膜7でもって改善し、面品位に優れた薄膜磁気ヘッド用基板1を提供する。

【0030】また、第1のアモルファスアルミナ膜7の厚みを0.2~2.4  $\mu$  m、好適には0.2~2.0  $\mu$  mに、第2のアモルファスアルミナ膜8の厚みを10~5500 Å、好適には10~5000 Åにするとよい。【0031】第1のアモルファスアルミナ膜7の厚みが0.2  $\mu$  m未満の場合にはポリッシュ加工が困難となり、絶縁特性が得られず、2.4  $\mu$  mを越えると放熱性が劣化し、素子のメディアへの接触が生じる。第2のアモルファスアルミナ膜8の厚みが10 Å未満の場合には絶縁特性が得られず、5500 Åを越えると膜の応力により剥離が発生する。

【0032】さらにまた、本発明においては、第1のアモルファスアルミナ膜7はスパッタリング法により形成した後に、その表面を滑らかに研磨するとよい。そのために、CMP加工をおこなって、AFMで測定する面粗度をRaで5Å以下にするとよい。

40 [0033]

【実施例】以下、本発明の実施例を説明する。出発原料としてアルミナ(純度 9.9%、原料粉末の平均粒径: $0.4\mu$ m)とチタンカーバイド(純度 9.5%、原料粉末の平均粒径: $0.3\mu$ m)を使用し、アルミナが 7.0 重量%、チタンカーバイドが 3.0 重量%の比率となるように秤量し、さらにチタンカーバイドに対し約 1.0 重量%の酸化チタンT  $i.O_2$  を添加し、そして、アルミナボールにて混合した。ついで混合粉末を成形し、1.6.0 0  $\infty$  、2.5 0 k g / c m  $^2$  の圧力で 1 時間ホットプレス焼成した。

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【0034】このようにして作製した焼結体をダイヤモンドホイールにより所定の円板形状に研削加工した後、ダイヤモンド砥粒を用いて表面のラッピング加工をおこなった。ついで、平均粒径 $0.5\mu$ mのダイヤモンドパウダーを用いて、基板表面と研磨板あるいは研磨布を相対的に摺動させて精密研磨をおこない、これによって基板の表面粗度Rae18Åとした。本実施例では上記研磨板として錫定盤を用いた。

【0035】そして、表1に示すとおり、純度99.5%のアルミナターゲットを用いてスパッタリング法にて、アモルファスアルミナを成膜し、その後、球状アルミナ微粉末を純水中に懸濁させた研磨液にて鏡面加工をおこなった後、球状セリア微粉末を純水中に懸濁させた研磨液にて最終精密加工をおこない、試料No.1~1\*

\*2のとおり膜厚 $1\sim4\,\mu\,m$ 、膜面表面粗度(Ra)3Å の第1のアモルファスアルミナ膜を形成した。

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【0036】しかる後、同表に示すとおり、試料No.7~12については、ECRスパッタリング法を用いて、膜厚を幾とおりにも変えた第2のアモルファスアルミナ膜を形成した。さらに第2のアモルファスアルミナ膜に代えて通常のスパッタリング法によりアモルファスアルミナ膜をつづけて成膜した場合を試料No.5および試料No.6として示す。

10 【0037】また、試料No.6、8、10については、球状セリア微粉末を純水中に懸濁させた研磨液にて精密鏡面加工をおこなった。

【0038】

試料 No		第1の アモルファスアルミナ膜 厚み(μm)	第2のアモルファスアルミナ膜		加熱処理	表面租度	抵抗値
			製法 (μm)	鏡面	後膜剝離	R a (Å)	Ω
*	1	4			無	3	1011
*	2	3		_	無	3	10°
*	3	2		-	無	3	109
*	4	1		_	無	3	10*
*	5	2	スパッタ (1 μ m)	無	無	1 2	1010
*	6	2	スメラッタ (0.3 μ m)	有	無	3	10 9
	7	2	ECR (5000 Å)	無	無	5	1013
	8	2	ECR (1500 Å)	有	無	3	1012
	9	2	ECR (100 Å)	無	無	4	1011
1	0	1	ECR (1500 Å)	有	無	3	1 0 1 2
1	1	1	ECR (50 Å)	無	無	4	1011
<b>*</b> 1	2	. 1	ECR (6000 Å)	無	有	6	1012

※印の試料Noは本発明の範囲外のものである。

【0039】これら各試料に対し、加熱処理後の膜剥離、表面粗度および抵抗値を測定したところ、同表に示すような結果が得られた。

【0040】加熱処理後の膜剥離については、各試料を真空雰囲気内で600℃の温度で加熱し、微分干渉顕微鏡(50倍)にて成膜段階の剥離状態を確認した。また、最外表面の表面粗度はAFMにて測定した。

【0041】常温抵抗値についてはTi/Auの電極を 膜面に20ヶ所/φ4マイクロインチ形成し、常温で印 50

加電圧10Vでもって三端子法を用いて膜表面と、基板の裏面との間の抵抗値を測定し、最低抵抗値を求めた。

【0042】表1に示す結果から明らかなとおり、本発明の試料 $No.7\sim11$ については、アモルファスアルミナ膜の厚みを $2.5\mu$ m以内にしても、抵抗値は10  $11\Omega$ 以上になり、優れた耐電圧が得られ、さらに加熱処理後に膜剥離が生じなくなり、表面粗度Raは5  $\Lambda$ 以下になった。

io 【0043】ECRスパッタによりアモルファスアルミ

ナ膜をつけると面粗さが大きくなる傾向があるが、その 反面、非常に高密度な膜が形成でき、成膜面の面粗度で もRalOAを越えない非常に平滑な面が得られた。な お、このような高密度膜であれば、СМР加工すること で、さらに平滑な面が得られる。

【0044】しかるに、試料No. 1~4から明らかな とおり、第1のアモルファスアルミナ膜だけである場合 には、 $4\mu$  m以上の膜厚を成膜しないと  $10^{11}\Omega$ 以上の 抵抗値が得られない。

【0045】また、試料No. 5、6から明らかなとお 10 り、2層膜にしても第2のアモルファスアルミナ膜をス パッタリング法により形成した場合であれば、試料N o. 2と試料No. 5とが示すように、同じ膜厚でも抵 抗値は高くなる傾向にあるが、膜厚3 μm以下では抵抗 値10<sup>11</sup>Ω未満となる。

【0046】さらにまた、試料No. 12のとおり、第 2のアモルファスアルミナ膜を6000Åの厚みで形成 した場合には、2層膜間の密度差による応力が高すぎる ために、真空中の加熱処理にて膜剥離が生じた。

#### [0047]

【発明の効果】以上のとおり、本発明においては、基板 上にスパッタリング法により形成した厚み 0.2~2. 4 μ mの第1のアモルファスアルミナ膜およびECRス パッタリング法により形成した厚み10~5500Aの 第2のアモルファスアルミナ膜とを順次積層したこと で、薄膜磁気ヘッド素子部の放熱性を上げるとともに、

素子のメディア面への接触を防止し、さらに膜密着強 度、電気的な耐圧、面品位に優れた薄膜磁気ヘッド用基 板が提供できた。

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【0048】また、本発明においては、本発明の薄膜磁 気ヘッド用基板を用いたことで、高品質かつ高信頼性の 薄膜磁気ヘッドが提供できた。

### 【図面の簡単な説明】

【図1】 (a) および (b) は本発明の薄膜磁気ヘッド 用基板を示す斜視図である。

【図2】図1 (a) における切断面線X-Xによる要部 拡大断面図である。

【図3】本発明の薄膜磁気ヘッドの層構造を示す要部拡 大断面図である。

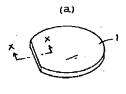
【図4】本発明の薄膜磁気ヘッドの使用状態を示す説明 図である。

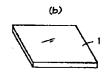
### 【符号の説明】

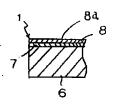
- 薄膜磁気ヘッド用基板 薄膜磁気ヘッド
- 3 スライダ
- 4 MR素子
- 20 メディア

  - 第1のアモルファスアルミナ膜
  - 第2のアモルファスアルミナ膜 8
  - 磁性膜

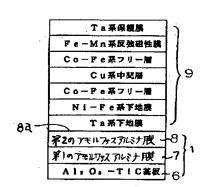
【図1】 【図2】







【図3】



【図4】

